L 8786-66

ACC NR: AP5028138

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the chain code is comparable to that of 10-digit group codes with R = 2 and approaches that of a tripled system (R = 3), where R is redundancy; (2) The chain code permits restoring information from check signals which helps in reserving the channels; (3) The chain code is expedient for simplex channels with an error probability P = 0.01-0.0001; with P > 0.01, the chain coding does not yield higher fidelity; with P < 0.0001, the chain coding may prove too expensive; (4) High detecting ability of the chain code and simplicity of the equipment required permit using it on automatic-RQ duplex lines; (5) The chain coding may prove useful in secondary-multiplexing systems working with parallel channels and frequency-time diversity. Orig. art. has: 4 figures, 14 formulas, and

SUB CODE: 17 / SUBM DATE: 12Feb65 / ORIG REF: 005 / OTH REF: 004

jw

Card 2/2

ACC NR: AP6009937

ACC NR: AP6009937

SOURCE CODE: UR/0118/65/000/011/0025/0026

AUTHOR: Bukhtiarov, V. A. (Engineer); Zhuk, I. N. (Engineer); Kulakov, N. N. (Engineer); Lozovoy, Ye. K. (Engineer); Malich, V. V. (Engineer); Napreychikov, F. I. (Engineer)

ORG: none

TITLE: Inductive relay for signaling, control, and telemetry

SOURCE: Mekhanizatsiya i avtomatizatsiya proizvodstva, no. 11, 1965, 25-26

TOPIC TAGS: electric relay, circuit design, telemetry equipment, automatic control equipment

ABSTRACT: The authors introduce a universal and stable inductive sensor which has a high degree of reliability and sensitivity. The inductive relay (sensor) proposed is intended for signaling, control, and telemetry. The device is based on a transistorized oscillator with tuned circuits in the base circuitry and on an emitter capable of operating in a "quasi-trigger" and intermittent oscillating mode. The all-purpose relay may be used in automatic control, monitoring and alarm systems, telemetry systems, and at unattended beacons. The output may be an electromagnetic relay or a contactless relay device of any type. The oscillator is distinguished by a high degree of frequency stability in all modes and uses a series-produced

UDC: 621.3.083:669.001.6

L 40909-66

ACC NR: AP6009937

P16 transistor (16 to 350 kc). The basic specifications of the inductive relay are: operating frequency: 25 kc; sensitivity: 150-200 mm; length of connecting wire to oscillator: up to 50 m; a 24-v dc MKU-48 relay; and a 220-v ac 50-cps feed voltage. Orig. art. has: 3 figures.

SUB CODE: 09/ SUBM DATE: 00/ ORIG REF: 000/ OTH REF: 000

L 39946-66

ACC NR: AP6014686

SOURCE CODE: UR/0108/65/020/012/0061/0064 2

AUTHOR: Bukhviner, V. Ye. (Active member); Istomina, G. V. (Active member)

ORG: Scientific and Technical Society of Radio Engineering and Electrocommunication (Nauchno-tekhnicheskoye obshchestvo radiotekhniki i elektrosvyazi)

TITLE: Discrete frequency and phase keyers (manipulators)

SOURCE: Radiotekhnika, v. 20, no. 12, 1965, 61-64

TOPIC TAGS: frequency shift telegraphy, phase shift telegraphy, radio telegraphy, carrier frequency, suctionic fullback, cutoff designing discrete frequency keyers and phase keyers that ensure high stability of subcarrier frequencies and high accuracy of deviation. To obtain a stable frequency keying without phase break, the use of a stable r-f oscillator with a controllable pulse-frequency divider is recommended; the pulse frequency should be a multiple of the marking rate; the feedback must be controlled by keying signals. During the release period, the divider output pulses are fed to its input via the feedback. The accurate phase keying can be obtained from a higher r-f oscillator with a controllable frequency divider; if the keying signals are unipolar, the phase-shift keying will result. Semiconductor logic elements are recommended for the above circuits. Orig. art. has: 5 figures and 5 formulas.

SUB CODE: 17,09 / SUBM DATE: 31May64 / ORIG REF: 005

Card 1/1 11b

UDC: 621.376.52

FUNERVI VERT, V. 19.

Ayadmronous start-stop regimerator for satio communication. Tost, syndam 25 no.5:18-34 lin 155. (Fib. 38:7)

1. Vedushchiy konstruktor Sanchaolissiedsvatelliskogo listimia. Ministerstva svygli ISM.

L 39116-66 EWT(d)/FSS-2 AP6030364 ACC NR: SOURCE CODE: UR/0106/66/000/005/0035/0042 40 AUTHOR: Bukhviner, V. Ye. ß ORG: none TITLE: Transformation of keying rates in transmission of discrete signals \mathcal{U}_{k} SOURCE: Elektrosvyaz', no. 5, 1966, 35-42 TOPIC TAGS: signal transmission, multichannel communication ABSTRACT: An analysis of problems of rate transformations in transmission of discrete signals in the coupling of single-channel wire line systems with multichannel systems of radio channel multiplexing. A circuit is presented for the rate transformer, and the basic parameters of the apparatus are noted. A method for alignment of the oscillators in a discrete synchronization system is suggested. The parameters of the transformation apparatus are determined by the parameters of the synchronization system. The authors recommend the usage of feedback from the output of the controlled divider to its input for periodic alignment of the frequency of the quartz oscillator in the discrete synchronization system. Orig. art. has: 4 figures and 2 tables. [JPRS: 37,061] SUB CODE: 17 / SUBM DATE: 06Sep65 / ORIG REF: 005 Card 1/1mir

L 08293-67
ACC NR: AP6032287 SOURCE CODE: UR/0106/66/000/009/0009/0017

AUTHOR: Bukhviner, V. Ye.; Malygin, V. B.

33 B

ORG: none

TITLE: Analysis of time distortions of digital signals in SW radio channels

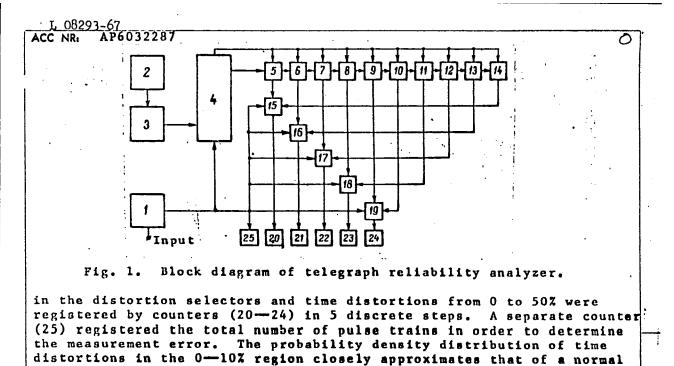
SOURCE: Elektrosvyaz', no. 9, 1966, 9-17

TOPIC TAGS: telegraph signal, signal shape, signal distortion, digital system

ABSTRACT: A study of time distortions of telegraph signals is described. Statistical measurements were made on 6 SW telegraph channels. The transmitter power was 20 kw and the receivers used broadside array antennas. A telegraph reliability analyzer was used to measure cumulative distortion. Receiver output (see Fig. 1) was applied to the analyzer input, where it controlled the formation of unipolar pulses. These pulses were applied to a synchronizing circuit (4) and distortion selectors (15—19). A crystal-controlled clock oscillator (2) and a buffer frequency divider enabled the synchronizing circuit to operate at various transmission speeds. Ten-stage pulse delay lines (5—14) formed reference pulses. The reference and input pulses were compared

Card 1/3 UDC: 621.391.833

Card 2/3



APPROVED FOR RELEASE: 06/09/2000 CIA-RDP86-00513R000307410010-5"

distribution; in the 15-50% region it approximates that of an exponential. Transmission quality was found to depend on the path

| ACC NRI AP6032287 direction; the highest quality was obtained for paths lying in meridian and south-to-east directions. Orig. art. has: 10 figures and 2 tables. | | | | | | | | | |
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Tashkent housing construction combine. Zhil.stroi. no.8:2-6
Ag '61. (MIRA 14:8)

(Tashkent--Precast concrete construction)

(Tashkent--Apartment houses)

BUKHVITS, K.I.

BUKHVITS, K.I.; PRYANISHNIKOV, S.K.

Remarks about the new textbook on the repair of flax-spinning machines ("Construction, assembly, repair, and adjustment of wet-spinning flax machinery."G.A.Sobol'ev. Reviewed by K.I. Bukhvits, S.K.Prianishnikov). Tekst.prom.14 no.12:50-52 D'54. (Spinning machinery)(Sobol'ev, G.A.) (MIRA 8:2)

BUKHVOSTOV, A., spets. red.; VYALKIN, A., red.; KUZIN, N., tekhn. red.

[Multiple machining of parts] Gruppovoi metod obrabotki detalei. Orel, Orlov koe knizhnoe izd-vo, 1963. 48 p.
(MIRA 16:12)
(Metal cutting)

31788 \$/056/61/041/006/036/054 B125/B102

24.6200

Bukhvostov, A. P., Shmushkevich, I. M.

TITLE:

AUTHORS:

ال أساد سد ..

Depolarization of negative muons in the production of muonic

atoms on spin-1/2 nuclei

PERIODICAL:

Zhurnal eksperimental'noy i teoreticheskoy fiziki, v. 41,

no. 6(12), 1961, 1895-1906

TEXT: The hyperfine structure of slightly excited levels in mesic atoms is assumed to be greater or equal to the level width. In the initial state where the hyperfine splitting is much smaller than the level width, the polarization remains constant. Subsequently, the muon falls to a level with a fine splitting that is great relative to the width. This applies also to all other levels traversed by the muon. At the end of this second stage, the muon polarization is about 1/3 in every finestructural state. In the F=O state, the muon is not polarized, and the mean spin of the meson on the K shell amounts to 3/4 of the mean spin in the F=1 state (F = total moment). The table contains the calculated values of the ratios denoted by β (polarization of the muon on the K shell

Card 1/6

Depolarization of negative ...

to the polarization at the end of the second stage). The last column summarizes the values of

 $\beta = \frac{1}{21+1} \beta_{1-1/2} + \frac{1+1}{21+1} \beta_{1+1/2}. \text{ The density matrices } \varrho^{(f)} \text{ and } \varrho \text{ in the final and initial state, respectively, are interrelated by } \varrho^{(f)}_{\nu\nu} = \exp\left\{-i\omega_{\nu\nu}, t\right\} \sum_{n} \frac{f_{\nu\mu}H_{\mu\nu}^{+}}{1+i(\omega_{\mu\mu}-\omega_{\nu\nu})\tau_{M}} \sum_{\epsilon\epsilon'} \frac{H_{\mu\epsilon}H_{\epsilon'\mu'}^{+}}{1+i(\omega_{\epsilon\epsilon'}-\omega_{\nu\nu'})\tau_{L}} \cdots \varrho^{(f)}_{\nu\nu}$

 $\cdots \sum_{\alpha\alpha'} \frac{H_{\beta\alpha}H_{\alpha'\beta'}^+}{1+i(\omega_{\alpha\alpha'}-\omega_{\nu\nu'})\tau_A} \rho_{\alpha\alpha'}.$

respectively. Here, $\boldsymbol{H}_{\alpha\beta}$ etc. denote the matrix element for the transition of the system from state α to state β with emission of a quantum or an Auger electron; τ_A and τ_B are the lifetimes of the levels A, B, ...; $\omega_{\beta,\beta}$, = $(E_p - E_{\beta})/\hbar$; E_{β} and E_{β} , are the energies of the sublevels β and β ! Card 2/6

Depolarization of negative ...

of the same group B; S indicates summation over the various cascades; we is the probability of the n-th cascade. The normalization factor \mathtt{N}_n is obtained from

 $SpQ^{(f_n)} = 1$. After averaging over time one finds

$$p^{(F_n)} = \sum_{n} w_n \rho^{(F_n)};$$

$$p^{(F_n)} = N_n D \left(\sum_{\mu\mu'} \frac{H_{\nu\mu} H_{\mu'\nu'}^+}{1 + i\omega_{\mu\mu'} \tau_M} \sum_{\epsilon\epsilon'} \frac{H_{\mu\epsilon} H_{\epsilon'\mu'}^+}{1 + i\omega_{\epsilon\epsilon'} \tau_L} \cdots \sum_{\alpha\alpha'} \frac{H_{\beta\alpha} H_{\alpha'\beta'}^+}{1 + i\omega_{\alpha\alpha'} \tau_A} \rho_{\alpha\alpha'} \right), \tag{3},$$

The symbol D indicates the elimination of elements for which $\omega_{yy} \neq 0$. For I = 1/2, the relation

$$\rho = N \left(1 + a_1 \mathbf{j} \mathbf{i} + n \left\{ a_2 \mathbf{j} + a_3 \mathbf{i} + a_4 \left[\mathbf{j} \mathbf{i} \right] + a_5 \left(\mathbf{j} \left(\mathbf{j} \mathbf{i} \right) + \left(\mathbf{j} \mathbf{i} \right) \mathbf{j} - \frac{2}{3} \mathbf{j} \left(\mathbf{j} + 1 \right) \mathbf{I} \right) \right\} \right), \quad (5)$$

is obtained for the group of states with definite n, 1, and j. a_i are card 3/6

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Depolarization of negative ...

$$N = (2j + 1)^{-1}(2I + 1)^{-1}$$
. In

$$\rho^{(F)} = \frac{1}{4} (1 + a_1^F \mathbf{j} \mathbf{l} + a_3^F \mathbf{n} \mathbf{F}) = \frac{1}{4} \left[(1 + \frac{1}{4} a_1^F + a_3^F \mathbf{n} \mathbf{F}) \mathbf{P}_+ + (1 - \frac{3}{4} a_1^F + a_3^F \mathbf{n} \mathbf{F}) \mathbf{P}_- \right] = \frac{1}{3} p_+ (1 + \frac{3}{2} \lambda^F \mathbf{n} \mathbf{F}) \mathbf{P}_+ + p_- \mathbf{P}_-.$$
(19),

 $P_{+} = (3 + 4\vec{j}\vec{l})/4$ and $P_{-} = (1 - 4\vec{j}\vec{l})/4$ are the operators of the projection on the F=1 and F=0 states, and

$$p_{+} = \frac{1}{4} \left(1 + \frac{1}{4} a_{1}^{F} \right), \qquad p_{-} = \frac{1}{4} \left(1 - \frac{1}{4} a_{1}^{F} \right). \tag{20}$$

are the probabilities of the corresponding states. The parameter $\lambda^F = (2/3)a_3^F/(1+(1/4)a_1^F) \text{ is equal to the polarization of the muon in the triplet state of the K shell. The depolarization coefficient } \beta_K = <\vec{s}_K \vec{n} > /<\vec{s}_K \vec{n} > reads$

$$\beta_{K} = \frac{a_{3}^{F}}{2\lambda} \frac{j+1}{j(j+1)-1(j+1)+3/4} = \frac{a_{3}^{F}}{2\lambda} \times \begin{cases} 1 & \text{if } j = 1+1/2 \\ -(j+1)/j & \text{if } j = 1-1/2 \end{cases}$$

Card 4/6

33.788

Depolarization of negative ...

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with $\beta_K=\sum_n w_n\beta_n$. In this sum, which goes over all cascades starting from the initial level, β_n denotes the depolarization coefficient for a definite cascade. For the transition of a muon from the initial state to the K shell,

$$a_{s}^{p} = a_{s}^{1} + \frac{4}{3} \sum_{i=0}^{l} \frac{l_{i}}{2l_{i}+1} \operatorname{Re} A^{(i)} (1-x_{i}), \qquad A^{(i+1)} = A^{(i)} x_{i} + \frac{1}{4l_{i}^{2}+1} (29)$$

is valid in the final state. Here the sum has to be taken over all intermediate levels in the respective cascade transition, and i=0, $(j_1=j)$. Two limiting cases are considered: (1) If the hyperfine splitting (except the K shell) is everywhere small compared to the level width, then

$$A^{(1)} = \frac{6\lambda}{2j+1} + \frac{12\lambda}{4j^2-1} = \frac{6\lambda}{2j-1}, \quad A^{(2)} = \frac{6\lambda}{2j-3} \text{ if } \tau. \text{ a.:}$$

$$A^{(i)} = \frac{6\lambda}{2j_1+1}, \quad A^{(j)} = 3\lambda,$$

$$(31).$$

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Depolarization of negative ...

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(2) If the hyperfine splitting is greater than the level width, then the depolarization on transition from a state with j=1+1/2 is about 4/3 less than in the first case. In the presence of a hyperfine structure, the muon consequently polarizes the nucleus during transitions between excited levels. Existing experimental data on the depolarization of muons on nuclei with I=1/2 (at present, only for P^{31}) confirm the theoretical considerations discussed here. There are 1 table and 11 references: 4 Soviet and 7 non-Soviet. The four most recent references to Englishlanguage publications read as follows: H. Überall. Phys. Rev. 114, 1640, 1959; M. E. Rose, Bull. Am. Phys., 4, 80, 1959; R. A. Mann, M. E. Rose. Phys. Rev., 121, 293, 1961; E. Lubkin, Phys. Rev., 119, 315, 1960.

ASSOCIATION:

Leningradskiy fiziko-tekhnicheskiy institut Akademii nauk SSSR (Leningrad Physicotechnical Institute of the Academy of Sciences USSR)

SUBMITTED:

July 6, 1961

Card 6/6

BUKHVOSTOV, A.P.; FRENKEL', V.Ya.

Temperature distribution in round and rectangular plates cooled by radiation in a vacuum at a given temperature along the plate's contour. Inzh.-fiz.zhur. 5 no.8:78-80 Ag '62.

(MIRA 15:11)

1. Fiziko-tekhnicheskiy institut AN SSSR imeni A.F. Ioffe, Leningrad.

(Heat--Radiation and absorption)

24.6610

s/056/62/043/002/040/053 B125/B102

AUTHORS:

Bukhvostov, A. P., Frenkel', V. Ya., Shekhter, V. M.

TITLE:

Disintegration of a photon into two photons in the nuclear

Coulomb field

PERIODICAL: Zhurnal eksperimental noy i teoreticheskoy fiziki, v. 43,

no. 2(8), 1962, 655 - 660

TEXT: Integrating the differential cross section for the disintegration of an incident low-energy photon into two photons in the nuclear Coulomb field over the angle ϕ between the planes $(\vec{k}\vec{k}_1)$ and $(\vec{k}\vec{k}_2)$ gives rise to

> (4) $d\sigma = Z^{2}\alpha^{5} \frac{\omega \omega_{1}^{3} \omega_{2}^{2}}{4\pi^{3} (45m^{4})^{3}} (278Y_{1} - 157Y_{2}) d\omega_{1} dx_{1} dx_{2};$

Card 1/5

Disintegration of a photon into...

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$$Y_{1} = -x_{1} - x_{2} - \frac{1}{2} \left(\frac{\omega_{1}}{\omega_{2}} x_{1}^{2} + \frac{\omega_{2}}{\omega_{1}} x_{2}^{2} \right) + \left[\left(x_{1} + \frac{\omega}{\omega_{1}} x_{2} \right) \left(x_{2} + \frac{\omega}{\omega_{2}} x_{1} \right) + \right. \\ \left. + \frac{\omega}{\omega_{1}^{3} \omega_{2}^{3}} \left(\omega_{1} x_{1} + \omega_{2} x_{2} \right) \left(\omega_{1}^{2} x_{1}^{2} + \omega_{2}^{3} x_{2}^{2} \right) \right] w^{-1/i} - \\ \left. - \frac{\omega^{2}}{2\omega_{1}^{4} \omega_{2}^{4}} \left(\omega_{1}^{2} x_{1}^{2} + \omega_{1} \omega_{2} x_{1} x_{2} + \omega_{2}^{2} x_{2}^{2} \right)^{2} \left(\omega_{1}^{3} x_{1} + \omega_{2}^{2} x_{2} + \omega_{1} \omega_{2} x_{1} x_{3} \right) w^{-1/i}, \right. \\ \left. Y_{2} = \frac{\omega_{1}}{\omega_{2}} x_{1} + \frac{\omega_{2}}{\omega_{1}} x_{2} - \left[\left(\frac{\omega_{1}}{\omega_{2}} x_{1} - \frac{\omega_{2}}{\omega_{1}} x_{2} \right)^{2} + \frac{\omega}{\omega_{1} \omega_{2}} x_{1} x_{2} \left(\omega_{1} x_{1} + \omega_{2} x_{2} \right) \right] w^{-1/i}, \right. \\ \left. w = \left(\frac{\omega_{1}}{\omega_{2}} x_{1} - \frac{\omega_{2}}{\omega_{1}} x_{2} \right)^{2} + 2 \frac{\omega}{\omega_{1} \omega_{2}} x_{1} x_{2} \left(\omega_{1} x_{1} + \omega_{2} x_{2} \right). \right.$$

$$(5).$$

The equation

$$\frac{d\sigma}{dx_1} = \frac{139Z^2\alpha^5}{60\pi^2} \frac{\omega^6}{(45m^4)^2}.$$
 (7)

results after integrating the differential cross section over x_2 with $x_1 = 0$ and integrating again over $\omega_1 \cdot x_1 = 1 - \frac{1}{kk_1}/\omega_1$; $x_2 = 1 - \frac{1}{kk_2}/\omega_2$; $x = 1 - \frac{1}{k_1} \frac{1}{k_2}/\omega_2$. $\frac{1}{k_1} \frac{1}{k_2} \frac{1}{k_1} \frac{1}{k_1} \frac{1}{k_2} \frac{1}{k_1} \frac{1}{k_2} \frac{1}{k_1} \frac{1}{k_2} \frac{1}{k_1} \frac{1}{k_$

8/056/62/043/002/040/053

Disintegration of a photon into...

momentum and energy of the incident photon; $\overrightarrow{k_1}$, $\overrightarrow{k_2}$ and ω_1 , ω_2 are respectively the momenta and energies of the final photons. Numerical integration, absolutely necessary for $x_{1,2}$, gives the angular distribution of one of the final photons with a fixed energy ω_1 when the direction of the other photons after impact is arbitrary (curves 1 to 4 in the Fig.). For small angles, the maximum for $\omega_1 \approx \omega_2$ corresponds to the maximum cross section for small q^2 ($q^2 = (\overrightarrow{k_1} + \overrightarrow{k_2} - \overrightarrow{k})^2$). This maximum shows up even more clearly when the momenta of both protons are fixed in direction. Integrating the differential cross section over the energy of the final proton results in the broken curve (5) and integrating this curve over the angle yields

 $\sigma = 12.2 Z^2 \alpha^5 \omega^6 / 4\pi^2 (45 m^4)^2 = 4.65 \cdot 10^{-36} Z^2 (\omega/m)^6 cM^2$. (8).

When Z = 80 and $\omega \approx m$ (m = electron mass), the cross section $\sigma \sim 3 \cdot 10^{-32}$ cm² is of the same order of magnitude as the photon-photon scattering cross

Card 3/

Disintegration of a photon into...

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section. The above results hold for negligible screening of the nuclear Coulomb field. When $\omega m \approx 1/137$, the cross section

$$\sigma = \frac{641}{3^{10}5^9\pi^2} Z^2 \alpha^5 (\omega a)^4 \frac{\omega^6}{m^8}. \tag{11}$$

obtained by allowing for screening, is equal to 0.41 $10^{-49} \text{Z}^2 \text{cm}^2$. When $\omega \leqslant 2\text{m}$, (8) is 2.5 times larger than the total cross section

$$\sigma \approx \frac{7 \cdot 139 (64 \ln 2 - 23)}{45^3 \cdot 2^9 \cdot \pi^3} Z^2 \alpha^5 \frac{\omega^6}{m^8}$$
,

calculated by the Weizsäcker-Williams method. For high energies one obtains $\sigma = \chi(2Z^2\alpha^5/\pi m^2)(\ln(\omega/m) - 1)$. There is 1 figure.

ASSOCIATION: Fiziko-tekhnicheskiy institut im. A. F. Ioffe Akademii nauk SSSR (Physicotechnical Institute imeni A. F. Ioffe of the Academy of Sciences USSR)

SUBMITTED: March 13, 1962

Card 4/6 (

BUKAI, J. M.; BUKHVOSTOV, A. P.; POPOV, M. P.

"Possible Experiments for the Determination of Pseudoscalar Contributions in $\mu\text{-Capture."}$

report submitted for All-Union Conf on Nuclear Spectroscopy, Tbilisi, 14-22 Feb 64.

FTI (Physico Technical Inst)

BUKHVOSTOV, A.P.; POPOV, N.P.

Capture of __mesons by polarized nuclei with spin 1/2. Zhur. eksp i teor. fiz. 46 no.5:1842-1852 My '64. (MIRA 17:6)

1. Fizko-tekhnicheskiy institut imeni A.F. Ioffe AN SSSR.

SKOROKHODOV, N.Ye., dotsent; KUCHKO, I.I., inzhener; KOROLEV, A.S.; SERKIN, M.G.; BUKHVOSTCV, I.G.

Investigation of the rolling of experimental rails. Trudy TSNII MPS no.111:25-32 '55. (MIRA 9:5)

BUKHVOSTOV, I.G.

Interfactory institute for the study and introduction of progressive work practices for the operation of soaking pits and blooming mills. Metallurg no.3:34-36 Mr '56. (MLRA 9:9)

1. Glavnoya upravleniya gosudarstvennoy metallurgichaskoy promyshlennosti tsentra i Vostoka Ministerstva chernoy metallurgii SSSR.

(Rolling (Metalwork))

BUKHVOSTOV, I.G.

130-7-23/24

AUTHOR: Bukhvostov, I.G.

TITLE: The Cornigliano Works in Genoa (Zavod Kornil'yano v Genuye)

PERIODICAL: Metallurg, 1957, Nr 7, pp.44-47 (USSR)

ABSTRACT: An account is given of the plant and products of the Cornigliano works in Italy. The plant includes sintering machines, coke ovens, blast furnaces, a steel melting shop, blooming mill, universal reversing four-high stand, a six-stand mill and a cold-rolling shop. There are 4 figures and 1 table.

AVAILABLE: Library of Congress.

Card 1/1

SOV/133-59-9-15/31

· AUTHORS: Belobrov, I.F., Bukhvostov, I.G. and Milikhin, A.Ye.

TITLE: Operation of 850/730/530 mm Continuous Billet Mill with

Vertical Rolls in the Chinese People's Republic

PERIODICAL: Stal', 1959, Nr 9, pp 812-817 (USSR)

ABSTRACT: A brief description of the above mill and its operation

is given. The equipment of the mill was designed and built in the USSR (Ref 1). Characteristic data of the individual stands - table 1; data on shears - table 2; roll passes - table 3 (Fig 3), table 4 (Fig 4) and table 5. It is stated that the mill is one of the

best of its type, suitable for mass production of a wide range of square and round billets. With some additional

equipment of the finishing part, the mill can be utilised for rolling of profiles (beams, angles etc).

The alternation of horizontal and vertical stands with individual drives from a d.c. variable rpm motor, permits

a large variation in the speed practice of rolls

(independently from their diameter) which should secure

production of high quality products. Mechanised adjustment of vertical and horizontal rolls enables a

Card 1/2 rapid transfer from one rolling line to another. The mill

SOV/133-59-9-15/31

Operation of 050/730/530 mm Continuous Billet Mill with Vertical Rolls in the Chinese Feople's Republic

> is considered as an important achievement of the Soviet and Chinese designers and machine-builders. There are 4 figures, 5 tables and 1 Soviet reference.

Card 2/2

PHASE I BOOK EXPLOITATION

SOV/3954

Bukhvostov, Nikolay Alekseyevich

- Kompleksnyy sposob resheniya energotekhnologicheskikh parametrov prokatki (Over-All Method for Finding the Power and Technological Parameters for Rolling) Moscow, Mashgiz, 1960. 113 p. Errata slip inserted. 2,200 copies printed.
- Reviewer: I.M. Pavlov, Corresponding Member, Academy of Sciences USSR; Ed.: Yu.L. Markiz, Engineer; Ed. of Publishing House: Yu.L. Markiz; Tech. Ed.: G.V. Smirnova; Managing Ed. for Literature on Heavy Machine Building (Mashgiz): S.Ya. Golovin.
- PURPOSE: This book is intended for engineers working in the design departments of machine-construction and metallurgical plants and also for those engaged in work on the automation of rolling mills.
- COVERAGE: This book contains material which makes it possible to establish the necessary and sufficient power of the principal engines, depending on a given gage and productivity, and also the optimal relationships and Card $1/\chi$

Over-All Method for Finding the Power (Cont.) SOV/3954 significance of the values of fundamental rolling parameters. In actual cases the book will help to detect and use hidden reserves of power and productivity. No personalities are mentioned. References are given in footnotes. TABLE OF CONTENTS: Introduction 3 Ch. I. Fundamental Power and Technological Rolling Parameters and Causes of Their Lack of Conformity 9 Ch. II. Fundamental Aspects and Formulas of the Complex Method 13 Ch. III Application of the Complex Method 32 Ch. IV. Stresses Arising in the Rollers of a Working Stand 54 Appendix 1. Analysis of the Technical Design of a Sheet Mill With a 2500 mm Hot Roller for One of the Metallurgical Plants, Using the Complex Method 73 Card 2/3

Over-All Method for Finding the Power (Cont.)

SOV/3954

Appendix 2. Determination of the Specific Consumption of Energy in the

Rolling of a Strip

93

AVAILABLE: Library of Congress

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AC/wbc/gmp 8-11-60

BUKHVOSTOV, I.G.; KHUAN SY-TSAN [Huang Sau-ts'ang]

¥j∜,

Expansion of rolling mill practices in the Chinese Peoples Republic. Metallurg 5 no.2:37-39 7 '60.

(MIRA 13:5)

(China--Rolling mills)

BUKHVOSTOV, I.G.

Introducing progressive practices in the planning and recording of the output of economical types of rolled products. Metallurg 9 no.5:27-28 My 164. (MIRA 17:8)

1. Gosplan SSSR.

BUKHVOSTOV, N., inzh.

Elements of large-panel buildings in seismic districts of Uzbekistan. Zhil. stroi. no.2:2-6 '62. (MIRA 16:1)

(Uzbekistan—Earthquakes and building) (Uzbekistan—Apartment houses)

BUKHVOSTOV, N. V., Cand of Tech Sci -- (diss) "Problems of earthquake proof buildings with walls made with simple construction." Tashkent, 1957, 14 pp (Institute of Construction, Academy of Sciences Uzbek SSR), 150 copies (KL, 32-57, 93)

BUKHVOSTOV, N.V.

Analysis of earthquake-caused building damage on the basis of
earthquakeproof construction principles. Biul. Sov. po seism.
no.3:137-150 '57. (MIRA 11:5)

no.3:137-150 '57.
(Ashkhabad--Earthquakes and building)

BUKHVOSTOV, N.V., inzh. Prinimali uchastiye: KOZEL, Yu.V., inzh.; BOL'SHEM, N.Ya., inzh., GORSKIY, G.Yu., kand.tekhn.nauk, red.; POZNYAKOV, A.P., red.izd-va; KAMINSKIY, M.P., tekhn.red.

[Temporary instructions on the use of lightweight walls built of solid bricks in earthquake-proof construction of houses and public buildings (VSN 02-58)] Vremennaia instruktsiia po primeneniiu sten oblegchennykh konstruktsii iz polnotelogo kirpicha v seismostoikom stroitel stve shilykh i grashdanskikh sdaiii (VSN 02-58).

Tashkent, Izd-ve Respublikanskogo proektnogo in-ia "Uzgosproekt," 1958: 67 p. (MIRA 12:6)

1. Uzbek S.S.R. Ministerstvo stroitel'stva. 2. Respublikanskiy proyektnyy institut "Uzgospreyekt" (for Bukhvostov, Kozel, Bol'shem).

(Walls) (Earthquakes and building)

6

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9.4300 (1137,1138,1143)

S/126/60/010/004/003/023 E073/E535

Lapkin, N.I., Bukhvostova, N. G. and Falaleyev, G.A.

AUTHORS: TITLE:

Influence of Heat Treatment on the Magnetic Properties

of Nickel-Zinc Ferrites γ PERIODICAL: Fizika metallov i metallovedeniye, 1960, Vol.10, No.4,

pp. 521-526

TEXT: The influence was investigated of the annealing (ferritizing) temperature of the mass and of the sintering (temperature of components on the initial permeability μ_0 , tg δ , the coercive force H_c, the residual induction B_r and the Curie point θ of nickel-zinc <u>ferrites</u> Vof the following composition by weight: Fe 0, - 66.0%, NiO - 12.0%, ZnO - 22.0%. The process of production of the specimens is briefly described. μ and tg6 were measured H_c , B_r and B_m were by means of a Maxwell bridge at 1000 cps, measured by a ballistic method. In the experiments over 500 toroidal specimens with an average diameter of 20 mm and a height of 5 mm were investigated. The first series of experiments were made for the purpose of determining the dependence of the magnetic properties and also the porosity of the tested nickel-zinc ferrites on the sintering temperature (1000 to 1350°C) for a constant Card 1/4

85037 s/126/60/010/004/003/023 E073/E535

Influence of Heat Treatment on the Magnetic Properties of Nickel-Zinc Ferrites

ferritizing temperature (1050°C) and a constant duration of the sintering process (4 hours). For a sintering temperature of 1100°C the magnetic properties proved very low (Fig. 1). With increasing sintering temperature up to 1250°C, the maximum induction and the initial permeability increased considerably and the coercive force and the loss angle tangent decreased. X-ray structural and metallographic analyses indicate that for a sintering temperature of 1250°C a solid solution of nickel-zinc ferrite is formed. Further increase in the sintering temperature leads to a change in the phase composition, namely, a decomposition of the zinc ferrite, an increase in porosity (Fig. 2) and poorer magnetic properties. The second series of experiments was made for determining the influence of the annealing temperature on the magnetic properties of ferrites sintered at 1250, 1300 and 1350°C; the results are plotted in Fig.3. The ferritizing process has a considerable influence on the shrinkage, the magnetic induction, the initial magnetic permeability and the loss angle. The coercive force is

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s/126/60/010/004/003/023 E073/E535

Influence of Heat Treatment on the Magnetic Properties of Nickel-Zinc Ferrites

only slightly affected by changes in the annealing temperature. Comparison of the results obtained on the influence of the annealing temperature of the mass and the sintering temperature of the finished components (Fig. 4) indicates that the process of ferritizing has a considerable influence on the magnetic properties The Curie point, 160°C, is determined by the chemical composition and does not depend on the heat treatment. The following optimum temperatures were determined: annealing 1050 to 1150°C, sintering not exceeding 1250°C. After annealing at 1050°C and sintering at 1250°C the tested ferrites had an initial permeability of 1000 to 1100 gauss/0e, tg& equalled 0.5 to 0.6. Such ferrites proved suitable as cores for surge transformers with surge durations of 0.6 to 1.0 µsec. For shorter pulses, ferrites with lower initial permeabilities and loss angles have to be used. Comparative tests with surge transformers have shown that ferrite cores are superior to cores of the magnetically soft alloys 79H5M (79N5M) and 50H(50N) By using ferrite cores it proved possible to reduce the weight and size of surge transformers by a Card 3/4

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S/126/60/010/004/003/023 E073/E535

Influence of Heat Treatment on the Magnetic Properties of Nickel-Zinc Ferrites

factor of 15 to 20, considerably reducing their cost and ensuring the obtaining of stable square topped pulses with steep fronts. There are 4 figures and 4 references: 3 Soviet and 1 English.

ASSOCIATION: Ural'skiy nauchno-issledovatel'skiy institut

chernykh metallov (Ural Scientific Research Institute

of Ferrous Metals)

SUBMITTED: November 14, 1959

Card 4/4

s/276/63/000/002/014/052 A052/A126

AUTHORS:

Lapkin, N.I., Krasnoperov, G.V., and Bukhvostova, N.G.

TITLE:

Investigation of heat treatment of soft magnetic alloys

PERIODICAL:

Referativnyy zhurnal, Tekhnologiya mashinostroyeniya, no.2, 1963, 61, abstract 2B270 (Tr. Ural'skogo n.-i. in-ta chern.

metallov, 1, 1961, 160-175)

TEXT: Heat treatment of Fe-Ni 50 H (50N), 79 HM (79NH) and Fe-Al 1016 (Yu16) soft magnetic alloys was investigated. Fe-Ni alloys were hot rolled on a 300 merchant mill. 50N and 79NM alloys after normalizing (heating to 1,050°C, holding 710 min, air cooling) and etching were cold rolled on a 6-roll mill with 87.5% reduction in area without intermediate annealing. The heat treatment of these alloys was carried out in an inertialess MNB-2 (MPV-2) vacuum furnace under different conditions: the annealing temperature was varied from 950 to 1,350°C, the holding from 0.25 to 3 hours, the rate of cooling in the 1,350-600°C range from 50 to 500°C/hour. From the temperature of 600°C the samples were cooled in a switched-off furnace at a rate from 100 to 5°C/min. Yu16 alloy was rolled to 0.35mm thickness on a

Card 1/2

Investigation of heat treatment...

S/276/63/000/002/014/052 A052/A126

2-roll hot rolling mill and then annealed in a saltpeter bath without protecting atmosphere under following conditions: temperature 800, 900, 1,000, 1,100 and 1,200°C, holding 1 hour, cooling to hardening temperature at a rate of 100°C/hour. The hardening temperature of Yu16 alloy was varied from 450 to 700°C. As hardening media water, 20% caustic soda solution and trans former oil were used. The effect of annealing and hardening temperature on the magnetic properties of 50N, 79NM and Yu16 alloys was determined as well as the effect of heat treatment on the thermal stability and ageing of these alloys. As a result of the investigations it has been established that the highest values of magnetic permeability can be reached for 50N allcy at an annealing temperature of 1,200-1,250°C and for 79NM alloy at 1,150-1,300°C. Tempering at ordering temperature (480°C) reduces the heterogeneity and increases the thermal stability of magnetic properties of 79NM alloy. The temperature of secondary recrystallization in 50N alloy is in the 1,200-1,400°C range. Yu16 alloy has the highest magnetic properties after annealing at 950-1,050°C and oil hardening at 650°C. There are 7 figures and 6 references. T. Kislyakova

(Abstracter's note: Complete translation.)

S/020/63/148/005/002/029 B112/B186

AUTHOR:

Bukhyalov, A. M.

TITLE:

Plotting of nomograms for first-genus equations with three

variables

PERIODICAL: Akademiya nauk SSSR. Doklady, v. 148, no. 5, 1963, 1005-1008

TEXT: The problem of plotting nomograms with one curvilinear and two rectilinear scales for an equation of the form

$$F(u_1, u_2, u_3) = 0 (1)$$

is reduced to the problem of transforming Eq. (1) into an equation of the

$$\begin{vmatrix} \mathbf{f}_{\alpha} & \mathbf{f}_{\alpha} & 1 \\ \mathbf{f}_{\beta} & 0 & 1 \\ \mathbf{f}_{\ell} & 1 & 1 \end{vmatrix} = 0. \tag{4}$$

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Plotting of nomograms for first-genus ... B112/B186

The results are

$$f_{\mu} = C_{\mu} I_{\mu} (u_{\mu}) = C_{\mu} \int_{\bar{u}_{\mu}}^{u_{\mu}} \frac{du_{\mu}}{\delta_{\mu 23} (\bar{u}_{\alpha}, u_{\mu})}$$
 (11)

$$f_{\alpha}(u_{\alpha}) = \frac{C_{\beta}C_{\gamma}I_{\beta}(\theta_{\beta}(u_{\alpha}, \overline{u_{\gamma}}))I_{\gamma}(\theta_{\gamma}(u_{\alpha}, \overline{u_{\beta}}))}{C_{\beta}I_{\beta}(\theta_{\beta}(u_{\alpha}, \overline{u_{\gamma}})) + C_{\gamma}I_{\gamma}(\theta_{\gamma}(u_{\alpha}, \overline{u_{\beta}}))},$$
(12)

$$\varphi_{\alpha}(u_{\alpha}) = \frac{C_{\beta}I_{\beta}(\theta_{\beta}(u_{\alpha}, \overline{u}_{\gamma}))}{C_{\beta}I_{\beta}(\theta_{\beta}(u_{\alpha}, \overline{u}_{\gamma})) + C_{\gamma}I_{\gamma}(\theta_{\gamma}(u_{\alpha}, \overline{u}_{\beta}))}.$$
(13)

The function $c_{\mu 33}$ is the determinant

$$g_{\mu}, \partial g_{\mu}/\partial u_{\mu}$$
 $(g_{\mu}/\partial u_{\alpha}, \partial^{2}g_{\mu}/\partial u_{\mu}\partial u_{\alpha})$

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S/020/63/148/005/002/029
Plotting of nomograms for first-genus ... B112/B186

where $g_{\mu}(u_{\alpha},u_{\mu}) = du_{\mu}/du_{\alpha}$.

ASSOCIATION: Belorusskiy politekhnicheskiy institut (Belorussian

Polytechnical Institute)

PRESENTED: April 20, 1962, by A. A. Dorodnitsyn, Academician

SUBMITTED: December 26, 1961

ASTAF YEV, N.N., kand.tekhn.nauk; MOROZOV, V.A., inzh.; BUKI, A.A., inzh.

Using nonlinear chains for the accurate measurement of current strength. Svar. proizv. no.10:33-35 0 163. (MIRA 16:11)

- 1. Kishinevskiy sel'skokhozyaystvennyy institut (for Morozov).
- 2. Institut energetiki AN Moldavskoy SSR (for Buki).

L 57852-65 EVI(h)/EWP(v)/T/EMP(t)/EWP(b)/EWA(c) PI'-1, JD/HM

ACCESSION NR: AP5012642

UR/0135/65/000/005/0014/0016 621.791.011:621.791.92

AUTHOR: Buki, A. A. (Engineer); Astaf'yev, N. N. (Candidate of technical sciences)

TITIE: On the causes of burnout of elements of the parent and filler metal in vibroar cuild-up welling A

SOURCE: Svarochnoye proizvodstvo, no. 5, 1965, 14-16

TOPIC TAGS: metal surfacing, vibroarc welding, filler electrodes, weld metal

ABSTRACT: Tests were made to determine the reasons for the burnout of steel components in build-up welding with a discontinuous arc, and methods for preventing the effect are discussed. It is shown that carbon burnout depends the probability of the burning time of the welding arc and that the longer the components of arc formula of the losses of tarbon during transfer of the filler metal time of arc formula of Manganese and silicon burnout depend basically on the total time of arc formula of elements is decreased. It is concluded that in order to increase the transfer of the components of an electrode wire to the build-up layer in vibroard welding it is

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L 57852-65

ACCESSION NR: AP5012642

necessary to decrease the arc burning and idle periods (increase the pulse frequency). Orig. art. has: 2 tables.

ASSOCIATION: Kishinevskiy sel'skokhozyaystvennyy institut im. M. V. Frunze

(Kishinev Agricultural Institute)

ENCL: 00

SUB CODE: MM

NO REF SOV: 011

OTHER: 000

BUKI, A.A.

Current integrator. Zhur.prikl.khim. 38 no.6:1398-1400 Je 165. (MIRA 18:10)

Paki, Fila

BIRO, Janos; BUKI, Bela; KOVACH, Arisztid.

Changes in higher nervous function after ischemic shock in rats. Kisérletes orvostud. 8 no.1:74-84 1956.

1. Budapesti Orvostudomanyi Egyetem Elettani Interete.
(SHOCK, exper.
ischemic, eff. on conditioned reflexes in rats (Hun))

(REFLEX, CONDITIONED eff. of ischemic shock in rats (Hun))

BUKI, B.

BIRO, J.; BUKI, B.; KOVACH, A. G. B.

Changes of the higher nervous activity following ischaemic shock. Acta physiol. hung. 10 no.2-4:277-289 1956.

Institute of Physiology, University Medical School, Budapest.
 (SHOCK, exper.
 ischemic, changes & restoration of CNS activity in rats following shock.)
 (CENTRAL NERVOUS SYSTEM, physiol.
 changes & restoration of activity following exper.
 ischemic shock in rats)

BUKI, Bela; BIRO, J.; DENES, Ivan; KOVACH, Arisztid;

Conditioned reflex method for experiments to be performed on several rats simultaneously. Kiserletes orvostud 9 No. 5-6: 545-550 Oct-Dec 58.

1. Budapesti Orvostudomanyi Egyetem Eletanni Intezete.

(REFLEX, CONDITIONED method for exper. performed on several rats simultaneously (Hun.)

BUKIB.
BIRO, J.; BUKI, B.; DENES, I.; KOVACH, A.G.B.

Higher nervous activity of adrenalectomized animals after ischzemia of the limbs. Acta physiol. hung. 14 no.1:45-56 1958.

RUSZNYAK, Istvan, akademikus; STARK, Ervin az orvostudomanyok kandidatusa; FOLDI, Mihaly, az orvostudomanyok doktora; BUKI, Bela; JUVANCZ Ireneusz, dr.; FISCHER, Janos, matematikus

Investigations in determining the effect of rutin and ascorbic acid on the capillary resistance in rats. Biol orv kozl MTA 13 no.1-2:1-10 62.

1. Magyar Tudomanyos Akademia Kiserleti Orvostudomanyi Kutato Intezete (for Rusznyak, Stark, Foldi, and Buki). 2. Magyar Tudomanyos Akademia Alkalmazott Matematikai Intezete Biometriai Csoportja vezetoje (for Juvanez).

*

KISFALUDY, Sandor; BUKI, Iela; MESZAROS, Sandor

Effect of oral amino acids on the ammonia concentration in the portal blood. Kiserl. orvostud. 16 no.4:385-390 Ag '64.

1. Budapesti Orvostudomanyi Egyetem I sz. Belklinikaja.

HUNGARY

HOLLO, Istvan, Dr. BUKI, Bela, Dr. FEHER, Tibor, Dr. KOREF, Oszkar, Dr; Medical University of Budapest, I. Medical Clinic (director: RUSZNYAK, Istvan, Dr) (Budapesti Orvostudomanyi Egyetem, I. Belklinika).

"Studies of Osteoporosis with Endocrine Correlations, IV. Postmenopausal Osteoporomalacia'."

Budapest, Orvosi Hetilap, Vol 107, No 13, 27 Mar 66, pages 591-593.

Abstract: [Authors' Hungarian summary] On the basis of i.v. Ca loading tests, the postmenopausal patients of the authors who suffer from bone atrophy were divided into two groups: true osteoporosis and "osteoporomalacia". It was pointed out that the two groups differ from each other not only with respect to the results of the Ca loading test but also in the excretion of the end products of androgen metabolism and possibly also in changes in the serum Ca and P level. On the basis of these studies, the use of androgenic hormones in the treatment of patients with "osteoporomalacia" does not seem to be sufficiently justified on theoretical grounds. 5 Hungarian, 11 Western references.

1/1

APPROVED FOR RELEASE: 06/09/2000 CIA-RDP86-00513R000307410010-5"

- 48 -

BUKI, G.; BUKKY, I.

"Mechanical equipment of the atomic power station in Calder Hall. Pt. 2, Thermal circuit and efficiency factor of the power plant."

p. 237 (Energia Es Atomtechnika) Vol. 10, no. 5/6, Aug. 1957 Budapest, Hungary

SO: Monthly Index of East European Accessions (EEAI) LC. Vol. 7, no. 4, April 1958

BUKI, G.

"Analytical and economic investigation of plutonium production in nuclear-power reactors." In English, p. 263.

PERIODICA POLYTECHNICA. (Budapesti Muszaki Egyetem) Budapest, Hungary Vol. 2, No. 4, 1958

Monthly List of East European Accessions (EEAI) LC, Vol. 8, No. 6, June 1959 Uncl.

H/008/60/013/04/06/009 B022/B014

AUTHOR:

Büki, Gergely

TITLE:

Problems of Water Processing in Atomic Power Plants /9

PERIODICAL: Energia es Atomtechnika, 1960, Vol. 13, No. 4-5, pp. 220-232

TEXT: Problems of water processing in atomic power plants must be studied separately for the cooling system of the reactor (primary cycle) and the cycle of the power plant (secondary cycle). Besides degassing and the formation of coatings, the following problems arise in connection with the primary cycle: 1) As a result of radioactive radiation, part of the light and heavy water circulating in the reactor decays into gases. 2) The permissible total quantity of salts in the cooling water of the reactor is considerably smaller than in the boiler water. 3) The occurrence of corrosion in power plant reactors may be ascribed to several causes. It is more dangerous than in boilers. 4) The water is activated by neutron bombardment. 5) The radioactive water from the primary cycle must be purified before it is discharged. The constantly permissible concentration of radioactive substances in water and air is

2

Card 1/3

Problems of Water Processing in Atomic Power Plants

H/008/60/013/04/06/009 B022/B014

given on the basis of recommendations made by the International Atomic Energy Agency (IAEA), and in accordance with the Drinking Water Standards of the USA and the NBS Handbook (No. 52, 1953). First, the author describes the effect of radioactivity on water as well as the decay of water (decay, recombination, increase in decay intensity in specific recombination rate $v_{\hat{R}}$). Experiments showed that the use of a recombinator is superfluous in the case of the 5 MW Soviet experimental atomic power plant. The relation $V_D = i_D \cdot G_r \, kg/mp$ (Fig. 1) holds for the water quantity (v_D) that decayed under the action of radioactive radiation on gases (cf. decay reactions). The degree of water decay in the EBWR reactor is shown in Fig. 2. Activation and other influences are dealt with next. Data on water activation are given in Table 2, while Table 3 supplies the pH and the water resistance as dependent on the concentration of nitric acid. In water-processing systems, a distinction is made between systems for water purification and systems for purification with water discharge (Fig. 3). Fig. 4 illustrates the operation of the former, and Fig. 5 that of the latter systems. Table 4

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Problems of Water Processing in Atomic Power H/008/60/013/04/06/009 Plants H/008/60/013/04/06/009

shows the part played by the principal isotopes in the activity of fission products at some time after fission. The procedures of purifying radioactive water, conventional techniques, reduction of radioactivity by chemical coagulation (Table 5), coagulation and precipitation (Table 6), and the influence of the pH of water upon the removal of Ru by means

of coagulation (Table 7) are thoroughly described. Other problems dealt with are the reduction of radioactivity by means of sand filtration (Table 8), addition of lime soda (removal of strontium, Table 9), evaporation, ion exchange (Tables 10, 11), phosphate coagulation (Table 12), addition of cermets (Table 13), and clay (Table 14). There are 5 figures, 14 tables, and 17 references: 4 Hungarian, 2 German, and 11 English.

ASSOCIATION: Budapesti Müszaki Egyetem Höerömüvek Tanszéke (Chair for Thermal Power Plants of the Technical University of Budapest)

Card 3/3

H/008/62/000/002/002/002 B123/B101

AUTHORS:

Büki, Gergely

TITLE:

Optimum thermodynamic parameters of reactor cooling

PERIODICAL: Energia és Atomtechnika, no. 2, 1962, 87 - 93

TEXT: This is the first part of a paper dealing with the entire coolant circuit of a reactor and with a few other problems related to reactor cooling, such as the temperature course in the coolant, or the ideal circuit at constant or varying coolant temperature. It is shown that the efficiency at constant coolant temperature is higher than at varying temperature. The optimum temperature curve of the fuel, which is determined by the neutron-flux distribution and the heating of the coolant, is examined. To improve the efficiency, it would be necessary to increase the temperature to an unlimited extent, which can only be achieved with the use of materials that are more favorable for nuclear-physical purposes. There are 5 figures.

Card 1/2

Optimum thermodynamic parameters ... H/008/62/000/002/002

ASSOCIATION: Budapesti Müszaki Egyetem Höerömüvek Tanszéke (Department of Thermal Energy, Technical University, Budapest)

Card 2/2

5.020

H/008/62/000/004/002/003 D249/D302

26.77(1 21.1000 AUTHOR:

Büki, Gergely

TITLE:

Optimum thermodynamical characteristics in reactor

cooling

PERIODICAL: Energia és atomtechnika, no. 4, 1962, 171 - 178

TEXT: In the first part of the paper the optimum temperature of the coolant leaving the reactor is investigated. A formula is deduced for the variation of the thermal efficiency as a function of the temperature of the coolant leaving the reactor, when the average temperature of the coolant is computed as the mean of its temperature on entry and departure on the T - S diagram. According to the relationship obtained, the increase of the thermal efficiency and the heat capacity decreasing on the reduction of the temperature difference will result in an optimum temperature for the coolant leaving the reactor. While in the case of coal fired generators this optimalization is not necessary, in the case of atomic reactors when the fuel temperature is maximum the increase of the coolant temperature on leaving the reactor would result in reduction Card 1/3

H/008/62/000/004/002/003 Optimum thermodynamical characteristics..D249/D302

of the amount of heat removed. The amount of heat removable is proportional to the surface transmitting the heat, the coefficient of heat transmission, and to the average difference between the temperatures of the fuel and coolant. The variation of the temperature difference is examined for: a) Evaporation cooling; b) liquid or gas cooling. The optimum coolant temperature on its departure from the reactor is investigated according to the following requirements: 1) To obtain maximum efficiency of the generator. 2) To obtain an econimical coolant temperature when the starting characteristics (temperature, pressure) do not vary with the load. In this case the optimum value of the coolant temperature is determined by the minimum cost of the unit of energy supplied by the generator. This has been the sole consideration in the case of coal fired generators where limitations in the maximum obtainable temperature were imposed by the structural materials. 3) In the case of nuclear generators introduction of a thermal cycle operating with initial characteristics which are variable as a function of the load may be advisable on thermodynamical grounds. The optimum heating of the reactor coolant is considered, assuming that: 1) The average temperature of the coolant is constant; 2) The temperature of the coolant is con-Card 2/3

stant when it leaves the reactor. Finally the thermodynamical properties of the ideal coolant and reactor cooling system are discussed. The paper contains a mathematical appendix. There are 7 figures and 5 references: 2 Soviet-bloc and 3 non-Soviet-bloc. The reference to the English-language publication reads as follows: A. Levai, et al, Mutual influences of nuclear power stations and cooperating power plant systems, World Power Conference Madrid, 1960, v. 7.

ASSOCIATION: Budapesti műszaki egyetem hőerőművek tanszéke (Technical University Budapest, Department of Heat Engines)

Card 3/3

BUKI, Gergely

Problems of water treatment in atomic power plants. Energia es atom 13 no.4/5:220-232 Ap-My '60.

1. Budapesti Muszaki Egyetem Hoeromuvek Tanszeke.

BUKI, Gergely

Role of efficiency of heat cycles in the economic appraisal of power plants of different types. Energia es atom 14 no.7:301-306 Jl '61.

1. Budapesti Muszaki Egyetem Hoeromuvek Tanszeke.

BUKI, G. (Budapest, XI., Stoczek u.4)

On thermodynamic fundamertals of reactor cooling. Periodica polytechn eng 6 no.2:129-145 62.

1. Lehrstuhl fur Warmekraftwerke, Technische Universitat. Vorgelegt von Prof.Dr. A.Levai.

BUKI, Gergely, adjunktus

Salt settling in steam superheaters and on turbine blades. Energia es atom 15 no.9:395-405 S '62.

1. Budapesti Muszaki Egyetem Hoeromuvek Tanszeke.

IEVAI, Andras, dr., Kossuth-dijas egyetemi tanar; BUKI, Gergely, muegyetemi adjunktus

** atom 15 no.12:527-544 D *62.

l. Magyar Tudomanyos Akademia levelezo tagja; Nehezipair miniszterhelyettes; "Energia es Atomtechnika" szerkeszto bizottsagi tagja.

BUKI, Gergely (Budapast, XI., Sztoczek u.2-4)

Thermodynamic principles of determining the geometric system of cooling cylindrical nuclear reactors. Periodica polytechn eng 8 no.1:43-56 '64.

1. Kafedra teplovykh elektrostantsiy Budapeshtskogo politekhnicheskogo instituta. Submitted June 6, 1963.

| | L 55885-65 EWT(1)/EWI(m)/EFF(c)/EFF(n)-2/EWG(m)/EPR Pr-4/Ps-4/Pu-4 WW/JW ACCESSION NR: AP4046513 B/0008/64/000/009/0433/0439 | |
|---|--|----------------|
| | AUTHOR: Buki, G. (Docent) | |
| | TITIE: Principles of the investigation and evaluation of reactor cooling thermodynamics Modynamics SOURCE: Energia es atomtechnika, no. 9, 1964, 433-439 | |
| 1 | TOPIC TAGS: nuclear reactor, plant material, shielding material, plant efficiency, steady load, reactor cooling system efficiency, thermal efficiency, electrical efficiency, optimal performance, maximum performance | |
| | ABSTRACT: This study analyzes the basic relations by which reactor cooling thermodynamics can be investigated and evaluated. These relations are useful in that with them reactor thermal efficiency and cooling efficiency may be obtained, and they would make it possible to design a reactor of ideal electrical efficiency, for these relations show that such reactor characteristics depend on reactor physics and heat engineering factors. In addition, by their proper application new ways of improving reactor cooling may be found. The three basic problems in reactor design are theoretically analyzed: 1) obtaining heat efficiency from the reactor; | r [*] |
| | Cord 1/2 | |

| efficiency which can be performance is often id where the limiting circ | ling system efficiency; 3) determination of the electrical realized with the reactor. It is pointed out that optimal sentical with maximum performance, especially in those cases sumstances of shielding and plant material do not alone demunstances are demunstances of shielding and plant material do not alone demunstances are demunstances and demunstances are demunstances are demunstances and demunstances are demunstances are demunstances. |
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| bility of making severe art, has: 40 formulas | and 9 figures. |
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| The same of the same of | Muszaki Egyetem Hoeromuvek Tanszeke, Budapest (Budapest Department of Heat Englises) ENCL: 00 SUB CODE: NP, TD OTHER: 007 |



"Reactor building raw materials with special regard to metals" by K.Lintner, E.Schmid.Reviewed by G.Buki. Periodica polytechn eng 6 no. 4:319-320 '62.

BUKI, Imre, okl.gepeszmernok

Examination of heat bransfer of liquid atomizers. (To be contd.) Energia as atom 15 no.2:49-54 F '62.

1. A Budapesti Muszaki Egyetem Hoeromuwek Tanszeke tudomanyos

11.7350

#/008/62/000/004/001/003 D249/D302

AUTHOR:

Büki, Imre

TITLE:

Examination of heat transfer in liquid atomizers. II

PERIODICAL: Energia és atomtechnika, no. 4, 1962, 145 - 151

TEXT: In the first part of the paper the methods of Giffen, Murashev and Novikov are appraised to determine the efficiency of eddy chamber atomizers. A new method is suggested for the calculation. A friction free flow and O overpressure all over the outflow orifice are assumed. The axial velocity was calculated from the energy equation of the liquid, when the tangential component originating from the free eddy was known. Radius of the air gap was assumed so large that under the given conditions the measure of outflow should be a maximum. The deductions resulted in a formula containing the efficiency in an implicit form. Determination from this is possible by graphical methods or by iteration, yielding satisfactory results in the case of industrial atomizers. The significance of this deduction is to provide information about the distribution of velocity in the film of liquid leaving the atomizer. Formulas are given for the va-

Examination of heat transfer in ...

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riation of the axial and tangential velocities in the outflow orifice. The sum of these velocity components is constant, but its direction changes along the radius within the thickness of the film of liquid. The direction of these velocities is such that the particles of liquid do not separate after leaving the atomizer, but form a continuous film. Shape of the film is determined by the mean direction of the departing liquid which can be calculated from the relation of the mean axial and tangential velocities. Not considering the effects of external forces, the shape of the film will be a hyperboloid of rotation; its geometrical measurements and their dependence on the measurements of the atomizer are described. The film of liquid is not stable, in which vibrations of different wave-lengths occur due to internal disturbances. These lead to cracking up of the film and its disintegration into droplets. Distance of disintegration measured along the axis of the atomizer will depend on the velocity of the outflow, the radius of the orifice, the density, viscosity and surface tension of the liquid. A formula is obtained for this length. The force of friction acting on the unit surface of the film is calculated. The heat transfer taking place in the film of liquid is investigated by the similarity of impulse Card 2/4

Examination of heat transfer in ...

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and quantity of heat exchange. As a result a formula is deduced for the factor of heat transfer as a linear function of friction force acting on the unit surface of the film. Finally the heat transfer taking place in the liquid mist is investigated. Applying the approximate formula derived here, the changes of the average temperature of the liquid mist can be found as a function of the time passed since the formation of droplets. Heat transfer taking place in the liquid mist is of less significance in the case of condensation. By applying formulas derived in this paper it can be found that the differences between the temperature of the vapor phase and that of the inflowing liquid — which is a possible measure of warming up — occurs to a considerable degree in the film phase. There are 2 figures and 23 references: 1 Soviet-bloc and 22 non-Soviet-bloc. The 4 most recent references to the English-language publications read as follows: A.H. Shapiro, A.J. Erickson, ASME, 79, no. 4, 1957, 775; K.P. Fraser, P. Eisenklam, Trans. Instn. Chem. Engrs., v. 34, 294, 1956; T. Karman, Collected Works, v. III, London, 1956; E. Giffen, A. Murashev, Atomization of Liquid Fuels, London, Chapman and Hall, 1953.

Card 3/4

Examination of heat transfer in ...

H/008/62/000/004/001/003 D249/D302

ASSOCIATION: Budapesti müszaki egyetem höerömüvek tánszeke (Technical University Budapest, Department of Heat Engines)

Card 4/4

OCSAI, Mihaly; BUKI, Imre

Calculating energy production costs of atomic power plants on the same principle. Energia es atom 13 no.3:124-134 Mr '60.

1. Eromu Tervezo Iroda (for Oqsai). 2. Muszaki Egyetem, Hoeromuvek Tanszek (for Buki).

H/008/62/000/002/001/002 B123/B101

AUTHORS: Büki, Imre, Mechanical Engineer, Scientific Co-worker

TITLE: Study of the heat transfer of atomizers

PERIODICAL: Energia és Atomtechnika, no. 2, 1962, 49 - 54

TEXT: This is the first part of an investigation conducted for the purpose of gaining a better insight into heat transfer which plays a significant role in the injection of liquid particles in the gas chambers of many chemical devices. The decomposition of a liquid into drops, the formation of a jet, and the influence of longitudinal and transverse vibrations in the jet are discussed. A high rate of outflow results in a considerable heat exchange, but the large diameter of the drops furnishes a small ratio of surface to volume. However, the drops formed after the dispersion of the jet are large, which is unfavorable from an economic point of view. The situation is more favorable with a liquid fan which is formed when two jets are directed to each other at a definite angle. The fan is thin, the surface-to-volume ratio is large, and a turbulent flow occurs inside. Whirling atomizers are discussed next, in which the liquid is set in Card 1/2

Study of the heat transfer of atomizers

H/008/62/000/002/001/002 B123/B101

turbulent motion before it flows out through the opening. The role of the drop phase must not be neglected, and the course of heat conduction in the drops must therefore be known. An attempt was made to determine the entire decomposition of liquid for any kind of atomization. Apart from lift and drag the motion of the liquid fog is governed by the laws of free fall. These effects are negligible in rotary condensers. There are 3 figures.

ASSOCIATION: Budapesti Müszaki Egyetem Höerömürek Tanszéke (Department of Thermal Energy, Technical University, Budapest)

Card 2/2

ACC NR: AR7004036 (4) SOURCE CODE: UR/0081/66/000/022/M005/M005

AUTHOR: Buki, Yu. M.; Filippova, Z. K.

TITLE: Effect of surface-active agents on the mechanical properties of high strength sintered corundum

SOURCE: Ref. zh. Khimiya, Part II, Abs. 22M34

REF SOURCE: (Sb. nauchn. tr.) Ukr. n.-i. in-t ogneuporov, vyp. 8(55), 1965,

TOPIC TAGS: corundum, sintering, surface-active agent, lubricant surface active. agent, mechanical property

ABSTRACT: The effect of the following surface-active agents on the strength properties of corundum ceramics has been investigated: water, H2SO4 and HCl solutions; paste based on secondary alcohols, oleic acid; self-emulsifying oil; and turpentine. The tensile strength of corundum ceramics is lowered most by water, oleic acid, self-emulsifying oil, and turpentine. In machining of corundum ceramics, surface-active agents are recommended for lowering the strength characteristics, for lubrication and for cooling. In practice, however, water and acids, being the

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ACCESSION NR: AP5002181

S/0032/65/031/001/0113/0114

AUTHORS: Buki, Yu. M.; Rutman, L. M.

TITLE: Determination of the limits of tensile strength for ceramic materials

SOURCE: Zavodskaya laboratoriya, v. 31, no. 1, 1965, 113-114

TOPIC TAGS: ceramic material, tensile strength

ABSTRACT: The method and apparatus are described by which the tensile strength of ceramic and other brittle materials can be measured. The samples are made in the form of thin-walled cylinders into which is introduced high-pressure liquid. From the basic laws of hydrostatics the pressure of the liquid is uniform at the boundary surface and is normal to it. Thus, uniform tangential tensile stresses are created in the wall of the cylinder. For thin-walled cylinders the tensile strength is given by

 $\sigma_{\rm D} = \frac{pr}{t}$

where p is the hydrostatic pressure at the moment of rupture of the sample, r is the radius of the cylinder, and t is the wall thickness. The mean square error in measurements using this method does not exceed 2.3%. Orig. art. has: $\frac{1}{2}$

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BUKI, Yu.M.

Ukrainian Conference on Industrial and Automatic Control Devices.

Priborostroenie no.9:32 S '62. (MIRA 15:9)

(Automatic control) (Ukraine--Production control)

BUKI, Yu.M.

"Assembly and operation of control and measuring instruments"
by M.D.Kuzin. Reviewed by IU.M.Buki. Prom.energ. 17 no.10:
51 0 '62. (MIRA 15:9)

(Automatic control) (Kuzin, M.D.)

LEVONTIN, L.I., inzh.; BUKI, Yu.M., inzh.

Pneumatic and electric level indicator for loose materials.

Mekh. i avtom. proizv. 17 no.8:44-45 Ag '63. (MIRA 16:10)

ROZHANSKIY, Z.Ye., inzh.; BUKI, Yu.M., inzh.

Automatic voltage limiter for the idling of welding transformers. Svar. proizv. no.1:34-35 Ja '64.

1. Khar'kovskiy stroitel'nyy tekhnikum.

(MIRA 17:1)

| L 53626-65 | |
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| ACCESSION NR: AP5016253 AUTHOR: Buki, Yu. M. (Engineer) * | UR/0122/64/000/011/0082/0083 |
| | ar on diamond tools and diamond finishing pro- |
| SOURCE: Vestmik mashinostroyeniya, no. | 11. 196). 82-82 |
| MOPIC TAGS: diamond, machine industry engineering conference, production eng | finishing machine, machine tool, mechanical |
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| stitute of Diamonds) on finishing bearing steels with diamond wheels, slabs and belts; Cand. of Tech. Sci, V. A. KHRUL'KOV and Engineer P. V. BERNT (Scientific Research Institute of Diamonds) on diamond finishing of crit. cal parts made of hard metals; Cand. of Technical Sci. M. S. NAYERMAN and Cend. of Tech. Sci. I. Ye. FRAGIN (Scientific Research Institute of Tractors and Agricultural Machinery) on experience in honing automobile and tractor parts with diamond slabs; Cand. Tech. Sci. V. A. FEDOTOV (Scientific Research Institute of Diamonds) on finishing of non-metallic experimental materials which would be impossible or extremely difficult without the use of a diamond tool; Cand. of Tech. Sci. L. K. FETROSYAN (State Committee on Machine Building) on comparative tests of natural and artificial diamond wheels; Engineer E. Ye. TSOFIN (Experimental Scientific Research Institute of Metal-Cutting Machine Tools) on modernization of existing machine tools and prospects for creating new ones for diamond grinding and finishing of metal cutting instruments) Engineer Y. ALFELY (State Committee on Machine Building) on diamond tools and attachments for bench work; Cand. of Tech. Sci. E. A. POPOV (MVTU (expansion not available)) on research to determine the coptimum concentration of diamond wheels; Engineer Ye. I. IZRAYLOVICE (Scientific Research Institute of Diamonds) on the | | |
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| V. V. VASILEVSKIY (Scient diamonds in wheel cutters | of application of diamond powder; Cand. of Tech. Sci. and cutters in the watchmaking industry; Engineer entific Research Institute of Diamonds) on the use of ers for cutting natural stone; Engineer I. P. I grinding and finishing of cutting tools in the | | |
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ROZHANSKIY, Zinoviy Yevseyevich; BUKI, Yuriy Markovich; ARAMCVA, L.I., dots., otv. red.; NESTERENKO, A.S., red.

[Practical laboratory work on the electrical equipment of substations] Laboratornyi praktikum po elektrooborudovaniiu podstantsii. Khar'kov, Izd-vo Khar'kovskogo univ., 1965. 120 p. (MIRA 18:5)

TASOVAC, Borivoj, prof. dr.; CALIC-PERISIC, Nada, dr.; BUKIC, Dragica, dr.

Viral pneumonia following influenzal infection and acute myocarditis. Med. Glas. 18 no.11:372-374 N $^{\circ}64$

1. Pedijatrijska klinika Medicinskog fakulteta Univerziteta u Beogradu (Upravnik: prof. dr. B. Tasovac)

KONECNI, Josin; PAVLOVIC-KENTERA, Vera; BUKICEVIC, Predrag; RADMIC, Sava

A case of congenital methemoglobinemia. Srpski arh. celok. lek. 89 no.10:1197-1201 0 161.

1. Interna klinika A Medicinskog fakulteta Univerziteta u Beogradu Upravnik: prof. dr Branislav Stanojevic.

(METHEMOGLOBINEMIA in inf & child)

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